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51	Abstract	In this paper, conventional simple methods of producing MMC with attained properties through the dispersion of silicon carbide in the matrix were investigated. To achieve these objectives two step-mixing method of stir casting technique has been employed. Aluminum (99.66 %C.P) and SiC (320 and 1200 grits) were chosen as matrix and reinforcement materials respectively. Experiments were conducted by varying weight fraction of SiC for 2.5 %, 5.0 %, 7.5 % and 10 %. The result indicated that the stir casting method was quite successful to obtain uniform dispersion of reinforcement in the matrix. This was evident by the improvement properties of composites over the base metal. Reinforced Aluminium Silicon Carbide (ASC) showed increase in Young's Modulus (E) and hardness above the unreinforced case and marginal reduction of electrical conductivity was recorded for the composites. The silicon carbide of 1200 grits (3 µm) showed increased Young's Modulus (E) and hardness of 1517.6 Mpa and 26.1 Hv values at 7.5 % volume fraction silicon carbide; when compared with the silicon carbide 320 grit (29 µm). Also; the electrical conductivity properties of the two grit sizes of the Silicon Carbides were less than the base metal for all the volume fraction of Silicon Carbide.
52	Keywords	Particulate - Aluminium composite matrix - Electrical properties - separated by ' - ' Silicon carbide
53	Foot note information	

1

2 **Aluminum Silicon Carbide Particulate Metal Matrix**  
3 **Composite Development Via Stir Casting Processing**

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Also; the electrical conductivity properties of the two grit 27  
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**Keywords** Particulate · Aluminium composite matrix · 30  
Electrical properties · Silicon carbide 31

**1 Introduction** 32

Metal matrix composite (MMC) is a range of advanced 33  
materials that are combinations of metal and hard particles, 34  
which are usually ceramics [1]. This product can be used for 35  
a wide range of applications. The MMC have superior to the 36  
base metal. These properties include improved thermal con- 37  
ductivity, abrasion resistance, tribology, creep resistance, 38  
dimensional stability, and exceptionally good stiffness. Like 39  
all composites, aluminum matrix composites are not a single 40  
material but a family of materials whose stiffness, strength, 41  
density, thermal and electrical properties can be tailored [2]. 42

According to Beffort [3], Aluminium Matrix Com- 43  
posites (AMC), are used for specific applications such 44  
as main cargo bay struts in space shuttle. The materi- 45  
al used was 6061/B/50f. Also, A359/SiC/20p is used 46  
for brake disks and drums; 2014/Al<sub>2</sub>O<sub>3</sub>/10-20p (Al-4.4Cu- 47  
0.5Mg-Si-Mn), 6061/ Al<sub>2</sub>O<sub>3</sub>/10-20p (Al-1.0Mg-0.6Si-Cu- 48  
Cr) and 7005/Al<sub>2</sub>O<sub>3</sub>/10p (Al-4.6Zn-1.4Mg-Mn-Cr-Zr-Ti) 49  
are used in bicycle frames, drive shafts and cylinder 50  
liner A357/SiC/10-20p (Al-7.0Si-0.5Mg), A359/SiC/10- 51  
20p (Al-9.0Si-0.5Mg), A339/SiC/10-20p (Al-12Si-1.0Mg- 52  
1.0Ni-2.25Cu), A360/SiC/10-20p (Al-9.5Si-0.5Mg) and 53  
A380/SiC/10-20p (Al-8.5Si-3.5Mg) are applicable in brake 54  
drums and brake discs; also while 6061/Al<sub>2</sub>O<sub>3</sub>/10p is 55  
used in automobile drive shaft; 6092/SiC/17.5p and 56  
2009/SiC/15p-T4 are used in fan exit guide vanes of Jet 57

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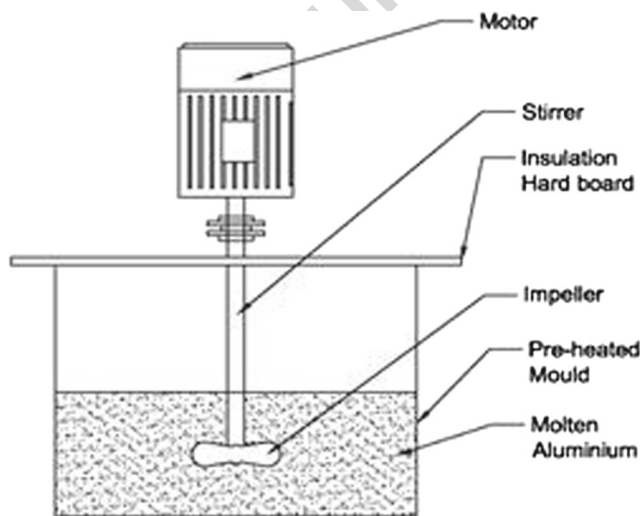
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58 engines and Al/Nextel610/45f is used for electrical conduc-  
59 tors.

60 Also an aluminium matrix composite processing route  
61 entails the using of aluminum as metal matrix with mixing  
62 particle to form composite, it has already found commer-  
63 cial use on account of the fact that conventional processing  
64 techniques such as powder metallurgy, vacuum hot press-  
65 ing, co-spray deposition process, squeeze casting, and stir  
66 casting methods can be readily adopted for the processing  
67 of such materials [4]. However, stir-casting method is pre-  
68 ferred to other methods because it is simple and processing  
69 parameters could be readily varied and monitored [5–7].  
70 The designed stir-casting system for this work is shown in  
71 Fig. 1.

72 In the production of liquid metal matrix composites, stir  
73 casting is generally accepted as a particularly promising  
74 route, currently practiced commercially [8]. By using this  
75 approach, there are many advantages such as simplicity,  
76 flexibility and can be used to produce large quantity of prod-  
77 uct. It is also attractive because in principle, it allows a  
78 conventional metal processing route to be used, and hence  
79 minimizes the final cost of the product [2]. The stir-casting  
80 technique is the most economical of all the available routes  
81 for metal matrix composite production [9], it allows very  
82 large sized components to be fabricated. The cost of prepar-  
83 ing composites material using a stir casting method is about  
84 one-third to half that of competitive method, and for high  
85 volume production, it is projected that the cost will fall to  
86 one-tenth [10].

87 In preparing metal matrix composites by the stir cast-  
88 ing method, there are several factors that need considerable  
89 attention. This includes, the difficulty of achieving a uni-  
90 form distribution of the reinforcement material, wet ability  
91 between the two main substances, porosity in the cast metal



**Fig. 1** The Schematic View of the designed Stirrer

**Table 1** The Compositions in Percentage of Aluminium Ingot Obtained from Aluminium Rolling Mills, Ota, Ogun State

Fe	Si	Mn	Cu	Zn	Ti	Mg	Pb	Sn	Al
0.232	0.078	0.000	0.0006	0.0016	0.006	0.0027	0.0012	0.007	99.66

92 matrix composites, and chemical reactions between the rein-  
93 forcement material and the matrix alloy [8]. In order to  
94 achieve the optimum properties of the metal matrix compos-  
95 ite, the following steps should be taken. The distribution of  
96 the reinforcement materials in the matrix alloy must be uni-  
97 form, the wettability or bonding between these substances  
98 should be optimized [6]. In order to overcome difficulty  
99 of achieving a uniform distribution of dispersion of silicon  
100 carbide particles in aluminium matrix, the help of two-step  
101 mixing method of stir casting technique was employed.  
102 For the wettability, the pre-treatment of the silicon carbide  
103 help in this direction and the tenacity of the bond between  
104 particles and matrix.

105 The focus of this study is to develop Aluminum Sili-  
106 con Carbide matrix composite, using stir- casting system.  
107 Also, the effect of silicon grit sizes on the mechanical and  
108 electrical properties on the material will be assessed.

**1.1 Materials and Methods**

109 In this work, stir-casting method was used to prepare sam-  
110 ples of AMCs using 1170Al reinforced with Silicon Carbide  
111 (SiC) particulates of 3 μm and 29 μm sizes respectively. The  
112 chemical composition of Aluminium and Silicon Carbide  
113 are presented in Tables 1 and 2 respectively.

114 The liquid metallurgy route (stir casting technique) was  
115 adopted to prepare the cast composites as described above.  
116 A batch of 5.0 Kg of 1170Al was melted at 750 °C in a  
117 graphite crucible using oil-fired tilting furnace for 25 min-  
118 utes. The temperature of the melt was measured using a  
119 K-type thermocouple. The molten metal was then poured  
120 into mould preheated at 450° f for 3 hours and the melt-  
121 ing was agitated with the help of stirrer to form a fine  
122 vortex. The SiC particles of 2.5wt% which was preheated  
123 at a temperature of 1100° C for 3 hours was added into  
124 the vortex with mechanical stirring at 500rpm according  
125 to Abbassipour et al. [2] for about 5mins. The experiment  
126 was repeated for different particle sizes (3 μm and 29μm)  
127

**Table 2** The Chemical Composition in Percentage of Silicon Carbide (SiC)

C	Al	Fe	Si	SiO <sub>2</sub>	Magnetic Iron	SiC
0.50	0.30	0.20	0.80	0.0016	0.04	97.6

**Table 3** The Mechanical and Electrical Properties of AlSiC Composite of different volume fraction of Silicon Carbide

S/N	Volume fraction Weight of SiC.	Grit Size	Modulus (N / mm <sup>2</sup> )	Yield Strength (MP <sub>a</sub> )	Hardness (H <sub>v</sub> )	Electrical Conductivity (MΩ / m)
1	2.5%	320 (29 μm)	1 233.87	28.51	21.56	66.35
		1200 (3 μm)	1293.43	35.45	23.95	67.84
2	5.0%	320 (29 μm)	793.22	27.21	21.41	61.85
		1200 (3 μm)	1028.56	33.69	23.60	67.70
3	7.5%	320 (29 μm)	1092.88	24.25	22.65	61.33
		1200 (3 μm)	1517.59	30.26	26.06	64.15
4	10%	320 (29 μm)	720.41	18.10	21.25	48.74
		1200 (3 μm)	878.93	22.25	25.90	56.63
5	Base Metal A11170	402.41	40.80	19.10	70.25	

128 and each size with different weight percentage (2.5, 5.0, 7.5  
129 and 10 wt %) of SiC were fabricated by the same procedure.

130 **1.2 Tensile Test**

131 All specimens produced through stir-casting method were  
132 cylindrical in shape and had dimensions of 110mm diameter  
133 and 30mm height. Five samples of each cast were cut out  
134 and prepared in the machine shop for tensile testing. Tensile  
135 test samples have cross sectional dimensions of 5mm  
136 by 10mm with a gauge length of 25 mm, were prepared for  
137 testing in Instron Universal Testing Machine (IUTM) with  
138 30 KN load. Five measurements (modulus) were taken for  
139 each sample and the average taken as the parameter value.

140 **1.3 Micro hardness Test**

141 Micro hardness measurements were carried out using a  
142 micro hardness tester. The micro hardness tester used was  
143 LECO 700AT with a load of 492.3mN and a dwell time of  
144 10 seconds. Before testing, specimen surfaces were polished  
145 using emery papers down to 1000 mesh. At least 6 measurements  
146 were taken for each sample and the average was taken as  
147 the micro hardness value.

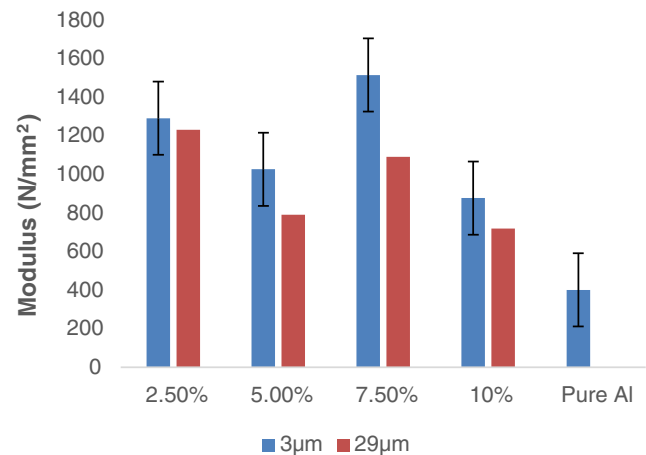
148 **1.4 Electrical Conductivity and Resistivity Test**

149 Samples of each cast were cut out and prepared for electrical  
150 conductivity testing. Test samples, having cross sectional  
151 dimensions of 5 mm by 10 mm with a length of 26 mm, were  
152 prepared for testing in 4 point probe machine. The working  
153 voltage of 20 mV was used. Voltage, current, resistivity and  
154 conductivity were obtained from the Keithley instruments  
155 model 2400.

**2 Results and Discussion**

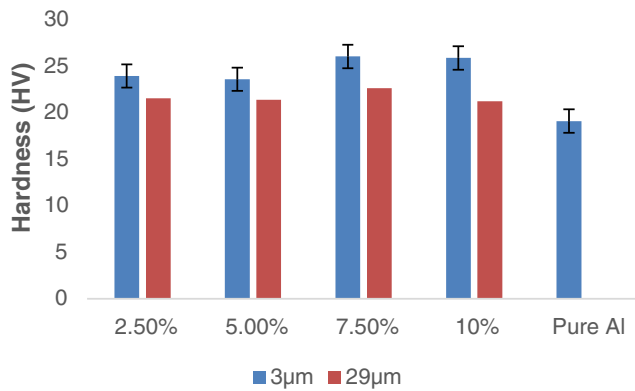
156  
157 Table 3 presents the mechanical and electrical properties of  
158 AlSiC composites of the two grit sizes of 320 (29 μm) and  
159 1200 (μm). The mechanical properties values were higher  
160 than the base metal aluminum. However, the electrical property  
161 values were marginally lower than the base metal. The results  
162 as indicated in Figs. 2, 3, 4, and 5, showed the increasing trend  
163 of modulus, hardness and yield strength with the lowest particles  
164 size of 1200 (3μm ) in weight percentage of Sic up to 7.5 %  
165 weight fraction.

166 The hardness of the composite was found to be considerably  
167 higher than that of the matrix alloy and increased with increasing  
168 particle content. The higher hardness of the composite samples  
169 relative to that of the matrix aluminium could be attributed to  
170 the existing hard particles (SiC) acting

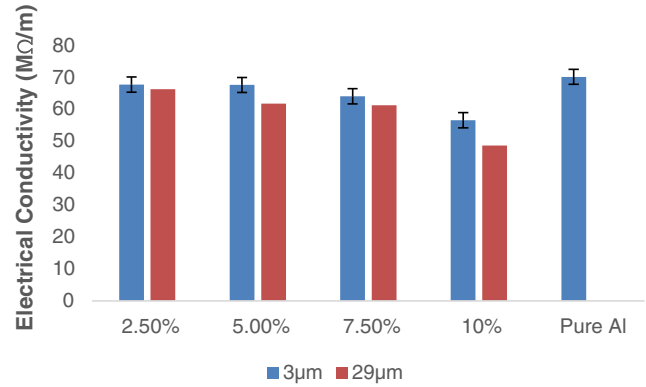


**Fig. 2** Comparative chart of modulus of elasticity of two grit sizes of Silicon Carbide particles





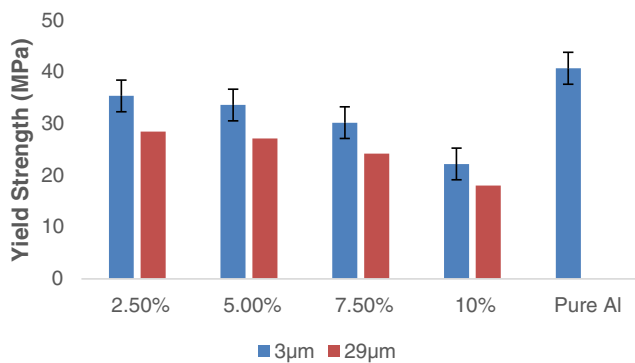
**Fig. 3** Comparative chart of Hardness of the two grit sizes of Silicon Carbide



**Fig. 5** Comparative chart of Electrical Conductivity properties of the two grit sizes of Silicon Carbide

170 as obstacles to the motion of dislocation. The Presence of  
 171 small separate particles in the microstructure can impede the  
 172 movement of dislocations provided that these particles are  
 173 stronger than the matrix in which they were embedded [11,  
 174 12]. The degree of strengthening produced also depends on  
 175 the size of particles, their distance apart and the tenacity  
 176 of the bond between particles and matrix. Also small grit  
 177 size of silicon carbide influenced the mechanical properties  
 178 [13].

179 The two step mixing, help to disperse the particles apart,  
 180 which results in to the strengthening produced by the small  
 181 size particle. When compared with the bigger particles, by  
 182 pre-heating, the silicon carbide at 1200°C for two hours  
 183 before the mixing probably helped tenacity of the bond  
 184 between the particles and the matrix, which added to the  
 185 strengthening effect. The particles of silicon carbides were  
 186 stronger than the matrix, the dislocation cannot pass through  
 187 them, and however the higher stress used during tensile  
 188 test might have activated the dislocation can by-pass them  
 189 leaving a “dislocation loop” around each particle. This will  
 190 make the passage of a second dislocations much more dif-  
 ficult, particularly since dislocations have greater difficulty



**Fig. 4** Comparative chart of yield strength behavior of the two grit sizes of Silicon Carbide

191 in passing between particles which are near to each other  
 192 resulting into higher strength of the small particle more than  
 193 the bigger one. The mechanical force by mixing mechani-  
 194 cally and pre-treatment of silicon carbide before the auto-  
 195 matic mixing was applied to overcome surface tension to  
 196 improve wettability.

197 The electrical conductivity of composite materials was  
 198 observed to be invariably lower than that of the monolithic  
 199 Aluminium-base metal. The electrical conductivity of com-  
 200 posite materials decreased with increase in particle sizes  
 201 and the volume percent of the reinforcement phase during  
 202 stir casting. However, the low material density of AlSiC  
 203 (3g/cm<sup>3</sup>) made it ideal for weight sensitive applications  
 204 such as portable devices over traditional thermal manage-  
 205 ment materials like copper molybdenum, CuMo, (10g/cm<sup>3</sup>)  
 206 and copper tungsten, CuW, (16g/cm<sup>3</sup>). [14].

207 Also, the addition of SiC molecules, a ceramic powder,  
 208 improved thermal stability of AlSiC material when com-  
 209 pared to the monolithic Aluminium. When this composite is  
 210 attached as a heat sink to an IC device, stress failure would  
 211 be avoided during service [14].

### 3 Conclusion

1. Simple designed conventional method of stir casting was used to produce Aluminium Silicon Carbide Composite. The metal matrix composite (MMC) materials produced show that modulus and hardness had higher values than the unreinforced base metal aluminium.
2. At 7.5 % volume fraction weight of silicon carbide of 1200( 3µm ) grit size have impressive mechanical properties when compared with other grit sizes.
3. There was marginal reduction of electrical conductivity for composite when compared with the base metal Aluminium.

225 4. The stir casting method seemed to disperse small grit of  
 226 silicon carbide in the matrix than the bigger grit, which  
 227 result in the improvement of the strength and mechanical  
 228 properties of the composite alloy. The small grit size  
 229 of Silicon Carbide influences the strength of mechanical  
 230 properties of the composites.

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